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Room-temperature heteroepitaxy of single-phase $Al_{1-x}In_xN$ films with full composition range on isostructural wurtzite templates

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Al_{1-x}In_xN heteroepitaxial layers covering the full composition range have been realized by magnetron sputter epitaxy on basal-plane AlN, GaN, and ZnO templates at room temperature (RT). Both Al_{1-x}In_xN single layers and multilayers grown on these isostructural templates show single phase, single crystal wurtzite structure. Even at large lattice mismatch between film and template, for instance InN/AlN (~13% mismatch), heteroepitaxy is achieved. However, RT-grown $Al_{1-x}In_xN$ films directly deposited on non-isostructural *c*-plane sapphire substrate exhibits a polycrystalline structure for all compositions, suggesting that substrate surface structure is important for guiding the initial nucleation. Degradation of Al₁. _xIn_xN structural quality with increasing indium content is attributed to the formation of more point- and structural defects. The defects result in a prominent hydrostatic tensile stress component, in addition to the biaxial stress component introduced by lattice mismatch, in all RT-grown Al_{1-x}In_xN films. These effects are reflected in the measured in-plane and out-ofplane strains. The effect of hydrostatic stress is negligible compared to effects of lattice mismatch in high-temperature grown AlN layers thanks to their low amount of defects. We found that Vegards' rule is applicable to determine x in the RT-grown $Al_{1-x}In_xN$ epilayers if the lattice constants of RT-sputtered AIN and InN films are used instead of those of strainfree bulk materials.

Keywords: AlInN, InAlN, sputtering, MSE, XRD, TEM, RSM, STEM

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I. INTRODUCTION

Since the bandgap of InN was revised to be in the infrared (IR) region (~0.7 eV) [1-6], Al_{1-x}In_xN alloys have become very important semiconductors due to their wide bandgap range, covering deep ultraviolet (UV) to IR. Hence, most of the semiconductor optoelectronics can possibly be fabricated from Al_{1-x}In_xN alloys, such as deep-UV laser diodes, infrared laser diodes, solar cells, high electron mobility transistors, solar-blinded photodetectors [7-14]. However, a wide-range composition immiscibility of the Al_{1-x}In_xN, in the range 0.1 < x < 0.9, impedes the fabrication of high-quality devices [15-18]. Phase separation of Al_{1-x}In_xN in the indium-rich region may occur when the growth temperature is higher than the InN dissociation temperature of 550 °C [1-4]. Besides, high temperature growth causes strong thermal stress in epitaxial films. Because the mismatch of thermal expansion coefficient between film and substrate, the in-plane strain of the epitaxial film can be changed from tensile to compressive during the cooling process, resulting in the formation of defects, cracks, and film peel off [19-21]. To suppress phase separation and eliminate thermal stress, films grown at room temperature (RT) are expected to eliminate these handicaps. Nevertheless, low growth temperature usually yields low crystalline quality of the films due to low mobility of adatoms. To overcome this disadvantage, the use of low-energy ion-assitance during epitaxial growth can be adopted to enhance the surface diffusion of adatoms [22-26]. Therefore, magnetron sputter epitaxy (MSE) [15,16,22] is a promising method for growing high-quality Al_{1-x}In_xN alloys of any composition at very low temperatures thanks to its inherent possibility of utilizing a high flux low-energy ionassistance.

Although RT-grown AlN epilayers have been demonstrated on different substrates, such as SiC and ZnO, by pulsed laser deposition and pulsed magnetron sputter deposition recently [23-25], RT-grown Al_{1-x}In_xN alloys covering the full composition range have not been explored. It is not sufficient to be limited to AlN as the choice of materials for many kinds of electronics. GaN and its ternaries is an option [27], but introduce additional difficulties in controlling the MSE process due to the low melting point of gallium. Hence, development of single-crystal Al_{1-x}In_xN ($0 \le x \le 1$) semiconductors is critical to explore more applications. However, growth of high-quality ternary Al_{1-x}In_xN is more difficult than the binary compounds since InN and AlN has a large lattice mismatch of ~ 13%, which is believed to be the reason for the wide solid miscibility gap. Therefore, defects can more easily be generated if adatoms do not occupy the host lattice points. Moreover, the lack of proper lattice-matched substrates also results in the formation of structural defects. The defects create a higher background carrier density and act as trapping centers in the epilayers, which may impede the fabrication of high-performance devices.

In this article, we report a study on single-phase 0002-oriented wurtzite $Al_{1-x}In_xN$ (0 $\leq x \leq 1$) single layers and multilayers epitaxially grown on isostructural substrates at RT by MSE. From an application point of view, we believe that the potential of fabricating high-performance opto-electronics using low-dislocation-density AlN, GaN, and ZnO substrates (commercialized availably) at RT is very high. Growing metastable $Al_{1-x}In_xN$ onto temperature sensitive substrates, e.g., indium-tin-oxide glass, plastic *etc*. by inserting a high quality seed layer is also desirable, which will vastly expand possible applications of group III-nitride semiconductors. For the fundamental physics viewpoint, investigation of the RT-heteroepitaxy using isostructural and non-isostructural substrates clarifies that substrate surface structure plays a vital role for the initial nucleation and film growth. Epitaxial film can be grown on isostructural substrates even with a large lattice mismatch between film and substrate. Through reducing lattice mismatch using a designed composition-graded multilayer, the quality of the as-grown film can be further increased. Deviations of lattice parameters

induced by strains and increase of structural mosaicity in the epilayers, as detected by highresolution x-ray diffraction (HRXRD), are due to the formation of point defects and extended defects which are confirmed by high-resolution transmission electron microscopy (HRTEM), scanning TEM ((S)TEM). Moreover, the applicability of Vegard's rule for these compounds is confirmed.

II. EXPERIMENTAL DETAILS

An ultra-high-vacuum (UHV) MSE deposition chamber equipped with two 50 mmdiameter and two 75 mm-diameter targets was utilized to grow Al_{1-x}In_xN alloys [15-17]. The chamber was evacuated to a base pressure of $< 4 \times 10^{-7}$ Pa with a combination of turbomolecular and mechanical pumps. High-purity 75 mm-diameter aluminum (99.999%) and 50 mm-diameter indium (99.999%) targets were used to either co-sputter ternary Al₁. _xIn_xN or sputter binary AlN and InN films under pure nitrogen ambient, supplied as pure nitrogen gas (99.999999%) achieved through a getter purifier. The substrates, including cplane sapphire, metal-organic chemical vapor deposition (MOCVD) grown GaN/Al₂O₃ and ZnO/Al₂O₃ templates, were degreased with trichloroethylene, acetone, isopropanol in ultrasonic baths for 5 min each and blown dry with pure nitrogen. High-temperature (HT) AlN/Al₂O₃ templates (HT-AlN) were grown in-situ at 1000 °C by MSE [8]. Prior to Al_{1-x}In_xN growth, the sapphire, GaN, and ZnO substrates were outgassed for 30 min at 1000, 800, and 700 °C, respectively. All Al_{1-x}In_xN single layers and multilayers were grown at RT. Typical dc-magnetron powers provided for indium and aluminum targets were of 10 and 50-350 W, respectively, to control the InN mole fraction. During the sputtering process, a pulsed substrate bias with the peak-to-peak potential of -20 to +5 V was applied to the sample holder to enhance growth by low-energy ion assistance.

The as-grown samples' structures were characterized in a Philips X'pert 4-axis materials research diffractometer with a Cu lab-source. For high resolution x-ray $2\theta/\omega$ scan (HRXRD) and rocking curve (XRC) measurement, the beam of pure Cu $k_{\alpha 1}$ (λ =0.15406 nm) radiation, produced through a parabolically curved graded multilayer mirror followed by a 2bounce symmetric channel-cut Ge(220) monochromater, was used as the primary optics, and a 2-bounce asymmetric channel-cut Ge(220) analyzer was used to collect the diffracted beam. For reciprocal space mapping (RSM), a 1° slit was used to achieve high intensities in both symmetric 0002 and asymmetric $10\overline{15}$ RSMs. The elemental compositions of the films were determined by Rutherford backscattering spectrometry (RBS) where 2.0 MeV ⁴He⁺ ions was used at an incident angle of 7° off from the surface normal to avoid channeling effects in the crystalline structure, [28] and back scattered ⁴He⁺ ions were detected at a scattering angle of 172°. Experimental data were analyzed by using the SIMNRA code (version 6.05) [29] to determine the Al_{1-x}In_xN composition. The concentration of elements as determined from Al₁₋ $_{x}In_{x}N$ single layers were used to calibrate the deposition fluxes from the magnetrons at various target powers. Microstructural analyses were performed by HRTEM, selected area electron diffraction (SAED), and (S)TEM using a FEI Tecnai G² TF 20 UT operated at 200 keV. The cross sectional TEM specimens were prepared by manual grinding and low-angle ion milling until electron transparency.

Figures 1(a) and 1(b) show schematic diagrams of single layers and multilayers $Al_{1-x}In_xN$ thin films, respectively. The growth conditions are listed in Tables 1 and 2, respectively. The single-layer samples consist of single $Al_{1-x}In_xN$ films grown on HT-AlN templates, which are labeled as $Al_{0.83}In_{0.17}N$, $Al_{0.65}In_{0.35}N$, $Al_{0.45}In_{0.55}N$, $Al_{0.28}In_{0.82}N$, and InN. The multilayer (ML) samples consist of multi $Al_{1-x}In_xN$ layers with increasing indium contents, from pure AlN or $Al_{0.83}In_{0.17}N$ to pure InN, grown on substrates of sapphire, HT-AlN, GaN, and ZnO templates, in this work denoted ML-sapphire, ML-AlN, ML-GaN, and ML-ZnO,

respectively. All samples were grown at RT except for a thicker 360-nm HT-AlN grown at 1000 °C, which exhibited lattice parameters equal to those of bulk AlN [20], $c_o^{AlN} = 0.498$ nm and $a_o^{AlN} = 0.311$ nm, as determined by RSM, and was used as a reference sample for strain determination in the seed layer. The compositions and thicknesses of the Al_{1-x}In_xN films shown in Table 1 were determined by RBS and TEM, respectively. Apparently, the aluminum content increases monotonically with magnetron power enabling a compositional control. For the multilayer samples, the magnetron powers of each layer are corresponding to those of single layers, shown in Table 1, with the sequence of AlN to Al_{1-x}In_xN multilayer to InN. Herein, the AlN layer was grown at RT.



Fig. 1. Schematic diagrams of (a) $Al_{1-x}In_xN$ single layer grown on a template with a HT-AlN seed layer, and (b) $Al_{1-x}In_xN$ multilayer grown on different templates, HT-AlN seed layer grown by MSE, GaN and ZnO seed layers grown by MOCVD.

Table 1 Growth conditions of RT-grown $Al_{1-x}In_xN$ ($0 \le x \le 1$) single layers (except samples HT-AlN-R and HT-AlN, which were grown at 1000 °C). All samples were grown on a ~ 40-nm thick HT-AlN seed layer.

Sample	Al power	In power	Composition,	Thickness
	(W)	(W)	X	(nm)
HT-AlN-R	350	0	0	360
HT-AlN	350	0	0	40
$Al_{0.83}In_{0.17}N$	350	10	17	132
$Al_{0.66}In_{0.34}N$	200	10	34	88
$Al_{0.46}In_{0.56}N$	100	10	56	100
$Al_{0.28}In_{0.72}N$	50	10	72	100
InN	0	10	100	87

Table 2 Templates used for RT-grown $Al_{1-x}In_xN$ ($0 \le x \le 1$) multilayers. The growth conditions of all subsequent layers were grown as the same as single layers listed in Table 1.

Sample	Template	First layer	subsequent layers
ML-sapphire	Al_2O_3	Al _{0.83} In _{0.17} N	$Al_{0.66}In_{0.34}N$ to InN (4 layers)
ML-AlN	HT-AlN/Al ₂ O ₃	Al _{0.83} In _{0.17} N	$Al_{0.66}In_{0.34}N$ to InN (4 layers)
ML-GaN	GaN/Al ₂ O ₃	RT-AlN	$Al_{0.83}In_{0.17}N$ to InN (5 layers)
ML-ZnO	ZnO/Al_2O_3	RT-AlN	Al _{0.83} In _{0.17} N to InN (5 layers)

III. RESULTS AND DISCUSSION

All $Al_{1-x}In_xN$ single layers show shiny surfaces and are transparent with colors changing from colorless (transparent), to orange, to brown, and to dark brown with increasing indium content, which implies the change of the energy band gaps from UV to near IR. However, the effect of point and structural defects in the $Al_{1-x}In_xN$ films can not be ruled out as a reason for the colorless to color transition owing to possible impurity/defect band absorption in the visible region. Since the carrier density of pure InN is still around 10^{20} cm⁻³, as determined by Hall measurements (not reported here), the absorption edge would be close to 1.6 eV owing to the Burstein-Moss (band filling) effect [1-3]. Hence, the InN film is expected to appear dark brown rather than black.

Figure 2(a) shows $2\theta/\omega$ -scan HRXRD patterns of the multilayer samples grown on the different templates. The film which was directly deposited onto sapphire (sample ML-Sapphire) can barely be detected by HRXRD. This material turned out to be polycrystalline with no epitaxial relationship, as determined by a combination of XRD techniques. When a HT-AlN seed layer, GaN or ZnO template was used, the HRXRD $2\theta/\omega$ exhibits strong peaks from each of the individual layers. All Al_{1-x}In_xN layers exhibit a single phase with growth orientation along the *c*-axis direction. Other crystalline orientations were not detected in longrange scans, even in low-resolution which allows for detection of polycrystalline materials. Apparently, the substrate structure is seen to play a very important role in the subsequent film growth. Although the atomic surface arrangement of *c*-plane sapphire has the same hexagonal geometry as wurtzite structure, the Al_{1-x}In_xN films did not grow epitaixally on sapphire. This growth behavior is completely different from HT growth where heteroepitaxy of III-N semiconductors on sapphire is commonplace. This is due to the relatively low kinetic energy at RT for adatoms to overcome the thermal barrier to reach the most stable sites. Therefore, the substrate surface structure (surface terminated layers) has to be considered as the reason of the growth difference. The wurtzite structure has a hexagonal close-packed (hcp) type (ABABAB....) stacking sequence with identical atomic arrangement for A and B layers. No matter if the nuclei occupy A or B terminated layers, the in-plane growth orientation and lattice-mismatch to the underneath layers of the nuclei are the same. Hence, the subsequently grown grains on these nuclei can all be *c*-axis oriented, but will eventually form domains defined by stacking mismatch boundaries. In contrast, sapphire is a rhombohedral structure



Fig. 2. (a) HR-XRD $2\theta/\omega$ scans of $Al_{1-x}In_xN$ multilayer (ML) grown on different templates. The thickness fringes are indicated by 'F' with arrows. (b) Top curve: $2\theta/\omega$ scan of an $Al_{0.28}In_{0.72}N$ single layer grown on HT-AlN layer. Bottom curve: Simulated curve of HT-AlN layer on sapphire. The dot lines are corresponding to the peak position of each thickness fringes in the simulated curve. (c) The 0002 reflections of $Al_{1-x}In_xN$ ML's rocking curves measured by sample ML-AlN. (d) FWHM of rocking curves. The InN mole fraction was determined from $Al_{1-x}In_xN$ single layers by RBS.

and does not possess the same stacking as wurtzite although it is often expressed in terms of hexagonal parameters. The structure viewed along the *c* axis shows hexagonal lattice, and the layer sequence follows with one O layer sandwiched in-between two Al layers [30-32]. The O layers follow approximately hcp-type stacking and Al layers follow face-centered cubic type (*abcabc*...) stacking. Since it is difficult to obtain an ideal well-terminated sapphire surface, the nuclei, which react to the Al and O terminated layers, will have different in-plane orientations (30° rotation) and lattice mismatches, for instance -35 and +13% for AlN on the Al and O terminated layers of the substrate, respectively. At low temperatures with strongly limited adatom mobility, this will limit the size of the subsequently grown grains in the film and new growth orientations, rather than *c*-axis, can develop and form polycrystalline structures or generally poor crystallinity.

The strain state of the sputtered films is discussed by comparing to the strain-free bulk materials [8,33,34]. Two indicating lines at 31.4° and 36.0° are plotted in the Fig. 2(a) to indicate the 0002 reflections of relaxed, stoichiometric InN and AlN, respectively. The XRD patterns show clear shifts of the AlN and InN reflections, possibly due to out-of-plane tensile strain, along the *c*-direction. Interestingly, the AlN peak shifts are in opposite directions depending on substrate material, indicating compressive and tensile strain along the *c*-direction, out-of-plane, for growth on GaN or ZnO and HT-AlN, respectively. However, the subsequent layers are located at the same positions except for the first layer of the Al_{0.83}In_{0.17}N, which apparently is strained in the same manner as the initial AlN layer. This result implies that the strain state of the Al_{1-x}In_xN layers subsequent to the second layer, may be relaxed. Nevertheless, all InN-peaks are shifted toward lower 20 angles as compared to strain-free bulk InN, indicating *c*-plane lattice expansions, independent of substrate. Such a positive out-of-plane strain may be an elastic reaction (aka. Poisson reaction) to an in-plane compressive biaxial stress (due to the effects of lattice and/or thermal expansion coefficient

mismatches) or an effect of a hydrostatic (spherical) stress component in the lattice (caused for example by point defects), or a combination of the two. The extra peaks (indicated by 'F') appearing around the first Al_{1-x}In_xN layer peak in the ML-AlN sample are thickness fringes from the HT-AlN due to the high-quality film with flat interfaces, as has previously been observed in similarly grown AlN [34]. Fig. 2(b) shows a $2\theta/\omega$ scan of the Al_{0.28}In_{0.72}N single layer on HT-AlN exhibiting the thickness fringes of the HT-AlN extending about -2° from the 0002 peak. A simulated curve generated by the Philips X'pert Epitaxy software shows that all fringes are well matched to the experimental data, assuming a thickness of the HT-AlN of 37 nm and ~ 1% in-plane compressive strain. The observed transverse lattice expansion, as reflected in the lower 0002 peak position compared to bulk AlN, may be a result of the elastic Poisson reaction. The mosaic tilts of those films were further characterized by XRC. Fig. 2(c) shows the rocking curves of the ML-AIN sample. The HT-AIN seed layer has an extremely narrow full-width-at-half-maximum (FWHM) of 0.02° (72 arcsec), which implies a very high quality of the layer. The following RT-grown Al_{0.83}In_{0.17}N layer also shows a narrow FWHM with a broad base profile. By fitting the curve to a two-peak Gaussian function, a narrow component with FWHM = 0.02° and a broad part with a FWHM of 0.54° are de-convoluted from each other. Hence, we conclude that the peak shape is attributed to a superposition of the narrow HT-AlN thickness fringes and the broader Al_{0.83}In_{0.17}N base profile. With increasing indium content, the FWHMs of the Al_{1-x}In_xN layers become broader, reaching 1.43° for the top InN layer. The FWHMs of all samples' rocking curves are plotted in Fig. 2(d). Both single layers and multilayers of $Al_{1-x}In_xN$ ($0 \le x \le 1$) show the same trend, where the FWHM increases with increasing indium content. Moreover, the FWHMs of highindium-content Al_{1-x}In_xN single layers are higher than from the corresponding compositions in the multilayer although they are grown on the high-quality HT-AlN seed layer. This difference shows that the lattice mismatch is a dominant factor in affecting the crystalline

quality rather than the previous layer's quality. For instance, InN, when directly deposited onto HT-AlN (with ~13% lattice mismatch [35]) has an XRC FWHM of 2.08° but only 1.43° if the InN is deposited on the lower quality Al_{0.28}In_{0.78}N layer with only 3% mismatch. Hence, minimizing lattice mismatch is important in isostructural RT heteroepitaxy for obtaining group III-N ternary material of highest possible structural quality.

Figure 3 shows RSMs around the symmetric 0002 and asymmetric 1015 reflections of samples ML-AlN [Fig. 3(a) and 3(b)], ML-GaN [Fig. 3(c) and 3(d)], and ML-ZnO [Fig. 3(e) and 3(f), where a log₂ scale of the contour levels has been used. All symmetric 0002 maps show well aligned contours along the transverse scattering vector (Q_z) direction for all Al_{1-x}In_xN layers. The centers of the contours are located at almost zero lateral scattering vector (Q_x) except for the top InN layers which show slight misalignments, indicating highly *c*-axis orientated growth of the films. In the asymmetric $10\overline{15}$ maps, the peaks can be seen to be well aligned along the $2\theta/\omega$ -scan direction, i.e., radially in reciprocal space except for the RT-AlN layers. Since AlN has the lattice mismatches of -2.3 and -4.3% to GaN and ZnO, respectively, the RT-grown AlN layers on GaN and ZnO templates exhibit in-plane strains, which are manifested as deviations from the $2\theta/\omega$ -direction in the RSMs in Fig. 3(d) and 3(f). In addition, only six peaks with 60-degree intervals were observed during azimuthal φ scans recording the $10\overline{15}$ reflections of any of the layers (not shown here), showing that the layers were grown in a highly oriented fashion with the epitaxial relationships of $(0001)_{f}$ (0001)_s and $[10\overline{1}0]_{f} \parallel [10\overline{1}0]_{s}$. From the above results, we can conclude that the Al_{1-x}In_xN layers were grown epitaxially on isostructural templates at RT. Next, the peak broadenings seen in both symmetric and asymmetric RSMs are analyzed in more details. The broadening that can be observed for the 0002 peaks, ellipsoidal contours, of the HT-AlN, GaN, and ZnO templates extend in the direction of the Ewald's sphere and is an artifact of using a receiving slit



Fig. 3. RSMs around the symmetric 0002 and the asymmetric 1015 reflections of $Al_{1-x}In_xN$ multilayers: (a) and (b) ML-AlN, (c) and (d) ML-ZnO, and (e) and (f) ML-GaN. Note: Logarithmic scale contour levels of RSMs were used in order to reduce the influence of strong intensity from GaN and ZnO templates. These maps were constructed with 2-axes $2\theta/\omega$ and ω scans. The axes of Q_z and Q_x are transverse and lateral scattering vectors, respectively. The length of Q is equal to $2\pi/d$, where d is the interplanar lattice spacing.

optimized for the less perfect $Al_{1-x}In_xN$ layers. The first layers, i.e., AlN or $Al_{0.83}In_{0.17}N$, also give raise to tilted ellipsoidal contours, indicating a high crystal quality. With increasing indium content, the 0002 peaks become broader and broader, implying a trend of degrading crystalline quality. In the asymmetric maps, the broadening can be further separated into to two types. One type is parallel to the lateral Q_x direction and is observed for the high Al content layers, $x \le 0.17$. This implies a short lateral coherence length owing either to growth with a characteristic column or domain width and/or the existence of laterally repeated structural defects such as misfit dislocations. The other type of broadening, which is parallel to the ω -scan direction and observed for high indium content layers, is attributed to mosaic tilts in the crystal lattice or a generally high amount of dislocations, grain boundaries, and/or point defects [6,36]. The maps show that higher indium content $Al_{1-x}In_xN$ layer contains more structural defects of the latter type.

Figure 4(a) shows *c* and *a* lattice constants of Al_{1-x}In_xN single layers and multilayers, extracted from RSMs, plotted as a function of InN mole fraction, as determined by RBS. The black solid and red dashed lines indicate strain-free lattice constants of Al_{1-x}In_xN, *c* and *a*, respectively, as predicted by Vegard's law using bulk AlN and InN lattice constants [20,21,35]. The experimental values of both *c* and *a* increase with increasing indium concentration and are longer than the strain-free lattice constants for all x > 0, revealing positive in-plane and out-of-plane strains. Only AlN layers show opposite in-plane and outof-plane strain states. In addition, the RT-sputtered InN layers have $a^{hN} = 0.356-0.358$ nm and $c^{hN} = 0.573-0.574$ nm, which are longer than the strain-free $a_o^{INN} = 0.354$ nm and $c_o^{InN} = 0.571$ nm [20,21], indicating that the InN plays the main role for producing the positive strains in sputtered Al_{1-x}In_xN films. Although the positive strains are presented in all Al_{1-x}In_xN layers (x > 0), the c/a ratios are still kept in the range of 1.600 to 1.613, which is in the range of strain-free AlN, 1.601, and InN, 1.613 [20,35]. In the present case, if the nominal bulk strain-free InN and AlN lattice constants are used to calculate the composition in the Al₁. $_x$ In_xN (x > 0) epilayers, an over estimation of the InN mole fraction is always obtained. In contrast, using the lattice constants of RT-sputtered InN and AlN, grown under the same conditions as the ternaries, the composition calculated from RSMs have a better match to the RBS result. Thus, we found that Vegard's rule, i.e., estimating the composition by linear interpolation of lattice parameters, is again applicable for all *x*. Hence, the strain state has to be taken into account for the composition estimation using XRD.



Fig. 4. (a) Lattice constants of $Al_{1-x}In_xN$ single layers and multilayer extracted from RSMs plotted as the InN mole fraction measured by RBS from $Al_{1-x}In_xN$ single layers. The solid and dash lines indicate ideal $Al_{1-x}In_xN$ lattice constants of *c* and *a*, respectively, and its relationship determined by Vegard's law from bulk AlN and InN lattice constants. *L-c* and *L-a* are lattice constants of *c* and *a*, respectively. (b) The calculated isotropic strain components, $\varepsilon_{ixa}(x)$, plotted as function of InN mole fraction.

To clarify the strain state in the Al_{1-x}In_xN layers, in-plane, $\varepsilon_1(x)$, and out-of-plane, $\varepsilon_3(x)$, strains are calculated by the following equations using the compositions determined from RBS and lattice constants, *a* and *c*, measured from RSMs.

$$\varepsilon_1(x) = 1 - \frac{x(a_o^{I \ n \ N} - a_o^{A \ I \ N}) + a_o^{A \ I \ N}}{a} \tag{1}$$

$$\varepsilon_{3}(x) = 1 - \frac{x(c_{o}^{I n N} - c_{o}^{A I N}) + c_{o}^{A I N}}{c}$$
(2)

If the film is under the elastic Poisson deformation with biaxial stress only, the ratio of $\frac{\varepsilon_3(x)}{\varepsilon_1(x)}$

is expected to be equal to $-\frac{2C_{13}(x)}{C_{33}(x)}$. Since the stiffness constants $C_{ij}(x)$ are dependent on c/a ratio as well as used calculation theories [37-39], making it difficult to present exact Poisson deformation, we adopt reliable stiffness constants calculated by Manuel and Morales *et al.* [38,39] using the method of Shapiro-Wilk statistical normality test for AIN and InN. There, the $C_{13}(x)$ and $C_{33}(x)$ are derived from Vegard's rule using stiffness constants of AIN, $C_{13}^{AIN} \approx 107$ and $C_{33}^{AIN} \approx 404$ GPa, and InN, $C_{13}^{InN} \approx 85$ and $C_{33}^{InN} \approx 237$ GPa. The calculated results show that all Al_{1-x}In_xN (x > 0) layers have positive strain ratios, indicating a predominantly hydrostatic internal stress, leading to a major isotropic strain component, in addition to a minor effect of a Poisson deformation only. Therefore, the measured total strain should contain all strain components and can be treated as the sum of the strain components: pure in-plane, $\varepsilon_1^*(x)$, and out-of-plane, $\varepsilon_3^*(x)$, strains, and isotropic strain component due to hydrostatic stress, $\varepsilon_{inc}(x)$ [40,41].

$$\varepsilon_1(x) = \varepsilon_1^*(x) + \varepsilon_{is.}(x) \tag{3}$$

$$\varepsilon_3(x) = \varepsilon_3^*(x) + \varepsilon_{is.}(x) \tag{4}$$

The isotropic strain component can be deconvoluted using Eqs. (1) and (2) and represented by Eq. (5),

$$\varepsilon_{is.a}(x) = \frac{2C_{13}(x)\varepsilon_1(x) + C_{33}(x)\varepsilon_3(x)}{2C_{13}(x) + C_{33}(x)}$$
(5)

Table 3 shows clear isotropic strain component presented dominantly in all $Al_{1-x}In_xN$ single layers. In contrast, the strain state of the HT-AlN seed layer is dominated by the Poisson deformation. Fig. 4(b) shows the isotropic strain component plotted as function of InN mole fraction for all samples. Obviously, the isotropic strain component is presented prominently in all RT-Al_{1-x}In_xN layers, but not HT-AlN layers. Although the scatter data increases with increasing indium concentration due to the broader peaks, shown in Fig. 3, the trend of the isotropic strain component still shows a clear increase with increasing InN mole fraction. The high value for the $Al_{1-x}In_xN$ layers with 0.72 InN mole fraction may be due to slight run-torun fluctuations in the growth conditions between the single layer depositions, used for RBS measurement, and the multilayer depositions.

Table 3 Strain state of the Al_{1-x}In_xN single layers. Measured in-plane, $\varepsilon_1(x)$, and out-ofplane, $\varepsilon_3(x)$, strains are calculated by using experimental values of both *c* and *a*, as well as compositions determined from RBS. The $\frac{\varepsilon_3^*(x)}{\varepsilon_1^*(x)}$ ratios are calculated from theoretical values, $-\frac{2C_{13}(x)}{C_{33}(x)}$. The calculated isotropic strain component shown in all Al_{1-x}In_xN layers

are much larger than HT-AlN.								
	<i>a</i> (nm)	<i>c</i> (nm)	In-plane strain, $\varepsilon_1(x)$	Out-of-plane strain, $\varepsilon_3(x)$	$\frac{\varepsilon_3(x)}{\varepsilon_1(x)}$	$\frac{\varepsilon_3^*(x)}{\varepsilon_1^*(x)}$	Isotropic strain, $arepsilon_{_{iso.}}(x)$	
HT-AlN	0.3089	0.5005	-0.0071	0.0048	-0.6733	-0.5297	0.0007	
$Al_{0.83}In_{0.17}N$	0.3200	0.5116	0.0050	0.0023	0.4573	-0.5501	0.0033	
$Al_{0.66}In_{0.34}N$	0.3274	0.5253	0.0052	0.0049	0.9273	-0.5738	0.0050	
$Al_{0.44}In_{0.56}N$	0.3386	0.5408	0.0103	0.0039	0.3783	-0.6110	0.0063	
Al _{0.28} In _{0.72} N	0.3458	0.5555	0.0110	0.0094	0.8492	-0.6441	0.0100	
InN	0.3585	0.5736	0.0126	0.0052	0.4167	-0.7203	0.0083	



Fig. 5. Cross-sectional bright-field TEM and STEM image of $Al_{1-x}In_xN$ multilayers grown on HT-AlN and ZnO seed layer: (a) and (b) ML-AlN and (c) and (d) ML-ZnO. The insets of Fig. 5(a) and 5(c) are the corresponding SAED patterns taken from samples ML-AlN and ML-ZnO, respectively. The corresponding zone axes of the film (all $Al_{1-x}In_xN$ ($0 \le x \le 1$) layers) and substrate are, $Al_{1-x}In_xN[1\bar{1}00]$ and Al_2O_3 [$11\bar{2}0$], and $Al_{1-x}In_xN[1\bar{1}00]$ and ZnO[$1\bar{1}00$], for sapphire and ZnO, respectively.



Fig. 6. Lattice resolved images of sample ML-AlN. (a) HT-AlN/sapphire interface, (b) $Al_{0.83}In_{0.17}N$, (c) $Al_{0.44}In_{0.56}N$, and (d) InN layers.

To get more insight into the origin of the obtained isotropic strain component in the films, HRTEM, STEM, and SAED were used to investigate the microstucture of the $Al_{1-x}In_xN$ multilayer samples ML-AlN and ML-ZnO, as is shown in Figs. 5 and 6. Bright-field TEM images, mass-thickness dependent dark-field STEM images, and SAED patterns are shown in Figs. 5(a)–(b) and Figs. 5(c)–(d) for samples ML-AlN and ML-ZnO, respectively. In the

bright-field images, the Al_{1-x}In_xN layers show prominent speckled contrast features, but the sapphire substrate shows even contrast, as shown in Fig. 5(a). This speckled contrast, which is due to the local strain field, shown in TEM images have been attributed to the formation of (clustered) point defects or small structural defects [42-44]. The dark to bright contrast transition from the bottom to the top layers, which is seen in the STEM image, corresponds to the transition from light AlN-rich to heavy InN-rich compounds. The STEM images further show rough interfaces between the Al_{1-x}In_xN layers and dense column-like domains. These columnar structures which are defined by domain boundaries throughout the layers become more emphasized as the indium content increase (though still epitaxial) and eventually develop as individual nanocolumns in the final InN layer. The insets of Figs. 5(a) and 5(c) show SAED patterns taken from the entire films including all layers as well as the part of sapphire substrate and ZnO, respectively. The Al_{1-x}In_xN reciprocal lattice points (RLPs) exhibit the same crystalline structure and orientation. The epitaxial relationships of the film (all $Al_{1-x}In_xN$ ($0 \le x \le 1$) layers) and substrate are confirmed to be, $Al_{1-x}In_xN$ $_{x}In_{x}N[1 \ \overline{1} \ 00] \| Al_{2}O_{3}[11 \ \overline{2} \ 0], Al_{1-x}In_{x}N(0001) \| Al_{2}O_{3}(0001)$ and Al_{1-} $_x$ In_xN[1100] $\|$ ZnO[1100], Al_{1-x}In_xN(0001) $\|$ ZnO(0001), for sapphire and ZnO, respectively. The shapes of the 0002 and $10\overline{1}l$ RLPs go from broadened laterally, i.e., in the Q_x direction, towards broadening circumferentially around the origin, as the indium content increases, which is consistent with the RSM results shown in Fig. 3. This is indicative of a transition towards material with generally poorer crystal quality with a larger degree of mosaic tilts/twists and with increasing amounts of lattice distortions [36].

Lattice resolved images of the HT-AlN, $Al_{0.83}In_{0.17}N$, $Al_{0.45}In_{0.55}N$, and InN layers in the ML-AlN sample are shown in Figs. 6(a)–6(d), respectively. Fig. 6(a) shows the interface between the HT-AlN seed layer and sapphire substrate. The HT-AlN exhibits a single-crystal

structure. Very few distortions from point- or small structural defects are observed in this part of the sample as is evident from the uniform lattice and even contrast. In the first $Al_{0.83}In_{0.17}N$ layer, shown in Fig. 6(b), a high-quality lattice image is observable, however, the amount of imperfections increase as is seen from the introduction of a more spot-like variation in the contrast, interpreted as local strain fields near point defects or small structural defects. A further inhomogeneous contrast is seen in the third $Al_{0.45}In_{0.55}N$ layer, shown in Fig. 6(c), where significant lattice distortions can be found locally. In the top InN layer [Fig. 6(d)], significant amounts of structural defects cause severe distortions of the lattice.

Hydrostatic stress observed in III-nitride semiconductors has been attributed to the existence of point defects, such as interstitials, vacancies, anti-site occupation, and substitutions in the film, as reported in previous literature [45-48]. Indium-rich nitride alloys have previously been shown to be very sensitive to inclusion of point and structural defects [49]. The reason for formation of point defects was referred to a large mismatch in the covalent radii of III-elements, indium (0.144 nm), gallium (0.126 nm), and aluminum (0.118 nm), and nitrogen (0.075 nm) [47-49]. Among point defects, the interstitials and anti-sites of indium at nitrogen positions can result in hydrostatic stress in the films. It has been shown that the interstitial nitrogen is dominant among those point defects in sputtered InN films [45,46]. In addition, the substitutions can contribute to structural defects when the elemental content of ternary alloys is within the miscibility gap. More defects appearing in the film is expected when the content of III-elements is close to equality. However, the structural quality of the Al_{1-x}In_xN films becomes worse as increasing indium content, and the InN films have even lower crystalline quality than all $Al_{1-x}In_xN$ (x < 1) films. The result indicates that the substitutions have a minor effect in contributing the defects in the Al_{1-x}In_xN films. Therefore we attribute the obtained isotropic strain component in the present Al_{1-x}In_xN lattices to be primarily associated with N-interstitials. The cause of such defects is likely the plasmasurface interaction where low energy nitrogen species (< 30 eV) may cause surface defects quenched into the growing crystal. We suggest that schemes for ion-assisted MSE, employing lower energies and higher fluxes, are explored for suppression of defect formation during growth in order to further improve crystalline quality.

IV. CONCLUSIONS

We have demonstrated RT heteroepitaxial growth of $Al_{1-x}In_xN$ ($0 \le x \le 1$) films on isostructural substrates, AlN, GaN, and ZnO, by MSE. All Al_{1-x}In_xN, including single layers and multilayers, exhibit single phase, single crystal wurtzite structure, and follow the orientation of the isostructural templates (substrates) well. The films with $x \le 0.17$ have the highest crystalline quality. However, Al_{1-x}In_xN films directly deposited on *c*-plane sapphire shows polycrystalline structure. We therefore conclude that isostructural substrate structure and small lattice mismatch are of critical conditions in determining the Al_{1-x}In_xN RT heteroepitaxy. Furthermore, multilayers with stepwise graded compositions, giving small lattice mismatch between subsequent layers, can be used for growing high-quality epifilms. Except for thin HT-AIN layers, the strain state presented in all Al_{1-x}In_xN layers is dominated by isotropic strain component rather than the Poisson deformation. The higher the indium content is in the Al_{1-x}In_xN films, the more defects are generated. The formation of point and structural defects are attributed to the introduction of InN. Using the strained InN of material grown under the same conditions as the ternaries, Vegard's law is still applicable to estimate composition for all x. The demonstrated RT heteroepitaxy of $Al_{1-x}In_xN$ by MSE is encouraging for its future application as an alternative material for high-performance electronics on sensitive substrates.

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